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CHAPTER 9

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UNIVERSITI TEKNOLOGI MALAYSIA

Malaysia's Premier University in Engineering and Technology

9.0 FARADAY'S LAW AND DISPLACEMENT CURRENT

Two topics will be discussed :

- (i) Faraday's Law – about the existence of electromotive force (emf) in the magnetic field*
- (ii) Displacement current – that exists due to time varying field*

*That will cause the **modification** of Maxwell's equations (in point form - static case) studied previously and hence becomes a **concept basic** to the understanding of **all fields in electrical engineering**.*

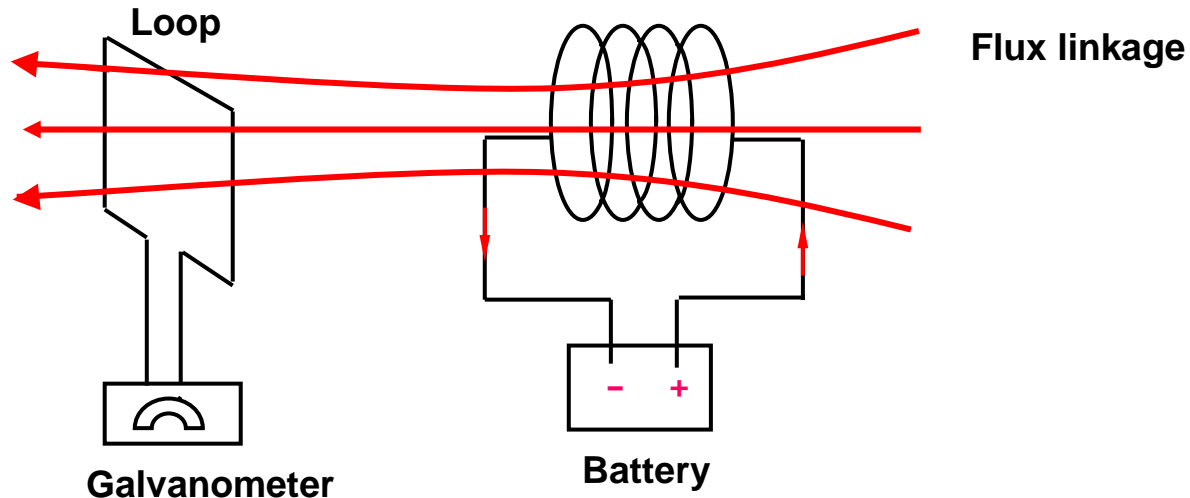
9.1 FARADAY'S LAW

Michael Faraday – proved that if the current can produce magnetic field, the reverse also will be true.

Proven only after 10 years in 1831.

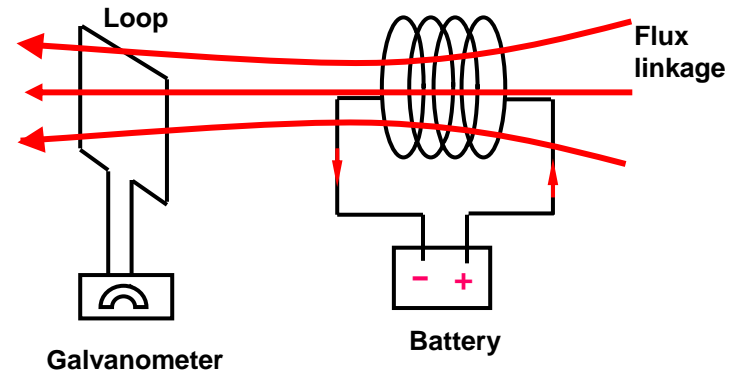
The magnetic field can produce current in a loop, only if the magnetic flux linkage the surface of the loop is time varying.

Faraday's Experiment :



- **Current produced magnetic field and the magnetic flux is given by :**

$$\psi_m = \int_s \vec{B} \cdot d\vec{s} \quad (1)$$



- **No movement in galvanometer means that the flux is constant.**
- **Once the battery is put off – there is a movement in the galvanometer needle.**
- **The same thing will happen once the battery is put on - but this time the movement of the needle is in the opposite direction.**

Conclusions : The current was **induced** in the loop

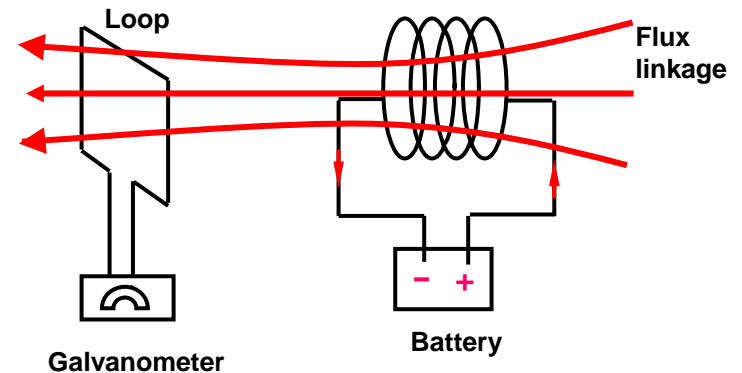
- when the flux varies
- once the battery is connected
- if the loop is moving or rotating

Induced current will induced electromotive voltage or induced emf V_{emf} given by :

$$V_{emf} = -N \frac{\partial \psi}{\partial t} = -N \frac{\partial}{\partial t} \int_s \bar{B} \cdot d\bar{s} \quad (V) \quad (2)$$

where $N =$ number of turns

Equation (2) is called *Faraday's Law*



Lenz's Law* summarizes the -ve sign is that : *The induced voltage established opposes the the flux produced by the loop.

In general, Faraday's law manifests that the V_{emf} can be established in these 3 conditions :

- Time varying field – stationary circuit (Transformer emf)***
- Moving circuit – static field (Motional emf)***
- Time varying field - Moving circuit (both transformer emf and motional emf exist)***

9.1.1 TIME VARYING FIELD – STATIONARY CIRCUIT (TRANSFORMER EMF)

$$V_{emf} = -N \int_s \frac{\partial \bar{B}}{\partial t} \cdot d\bar{s} \quad (V) \quad (3)$$

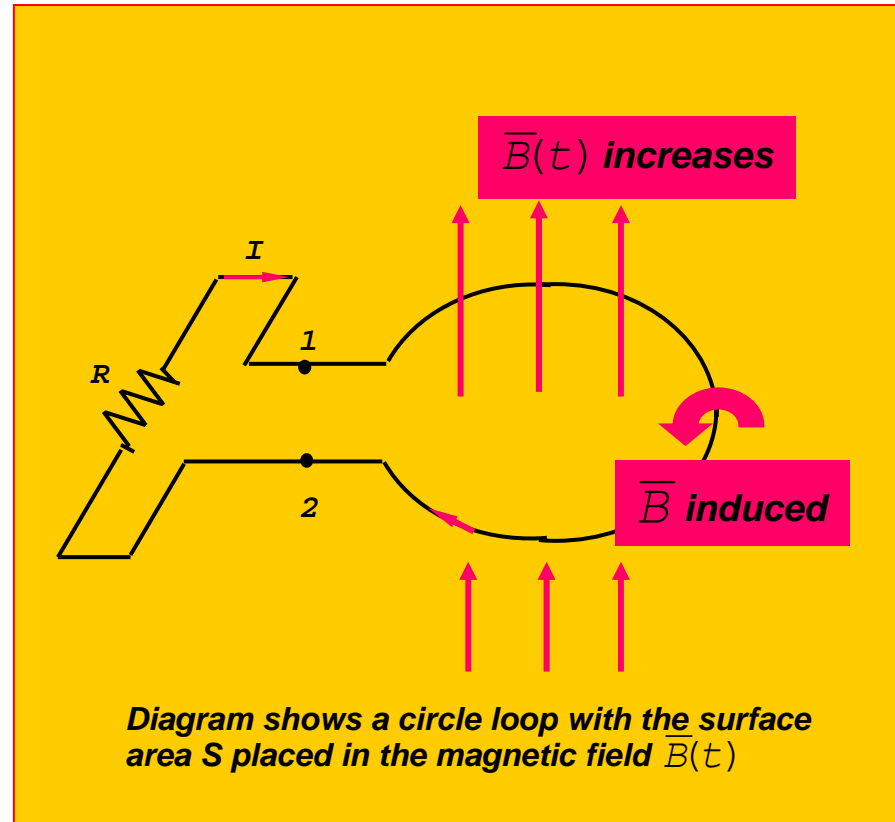
V_{emf} = the potential difference at terminal 1 and 2.

From electric field :

$$V_{emf} = \oint_{\ell} \bar{E} \cdot d\bar{\ell} \quad (4)$$

If $N = 1$:

$$V_{emf} = \oint_{\ell} \bar{E} \cdot d\bar{\ell} = - \int_s \frac{\partial \bar{B}}{\partial t} \cdot d\bar{s} \quad (5)$$



$$V_{emf} = \oint_{\ell} \bar{E} \cdot d\bar{\ell} = - \int_s \frac{\partial \bar{B}}{\partial t} \cdot d\bar{s}$$

Using Stoke's theorem :

$$\int_s (\nabla \times \bar{E}) \cdot d\bar{s} = - \int_s \frac{\partial \bar{B}}{\partial t} \cdot d\bar{s} \quad (6)$$

Hence Maxwell's equation becomes :

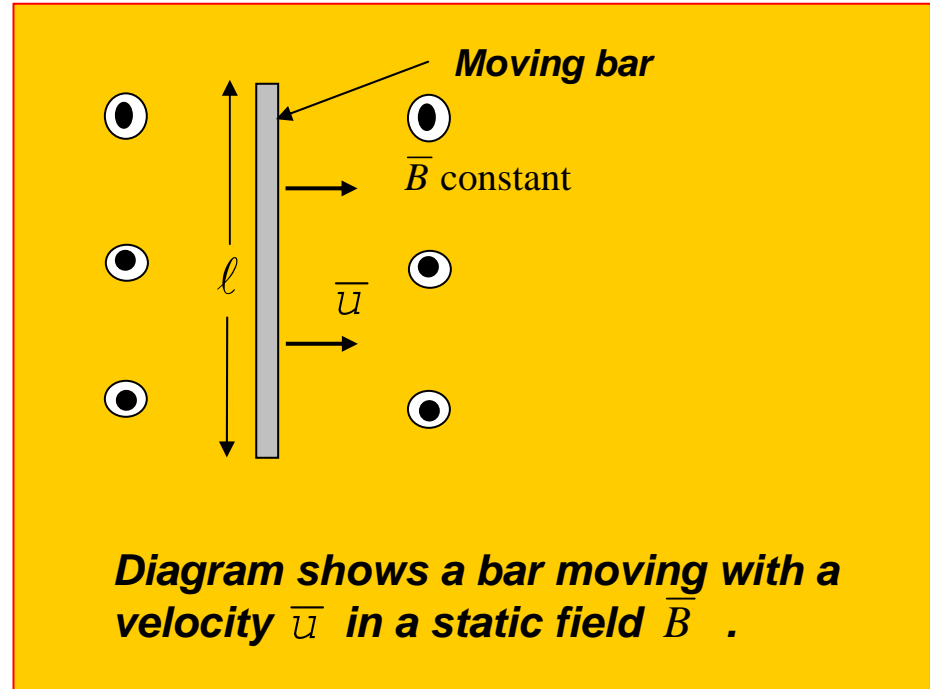
$$\nabla \times \bar{E} = - \frac{\partial \bar{B}}{\partial t} \quad (7)$$

9.1.2 MOVING CIRCUIT – STATIC FIELD (MOTIONAL EMF)

Force :

$$\bar{F}_m = q (\bar{u} \times \bar{B})$$

$$\bar{E}_m = \frac{\bar{F}_m}{q} = (\bar{u} \times \bar{B})$$



Hence :

$$V_{emf} = \oint \bar{E}_m \cdot d\bar{\ell} = \oint (\bar{u} \times \bar{B}) \cdot d\bar{\ell}$$

Fleming's Right hand rule

Thumb – Motion

1st finger – Field

Second finger - Current

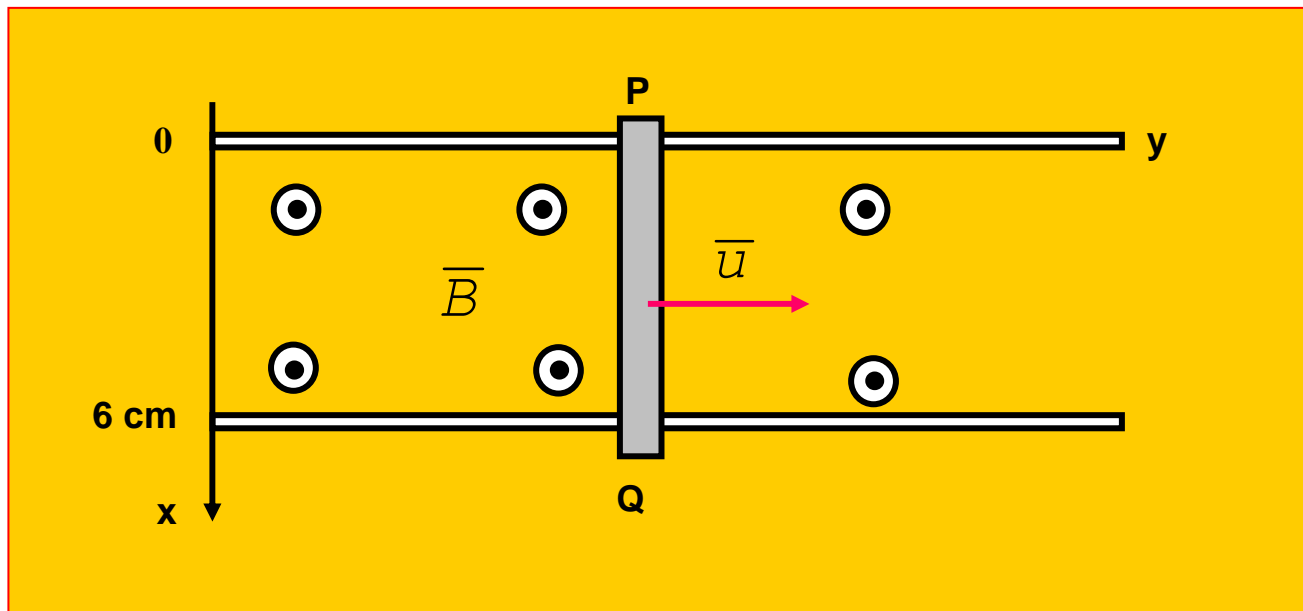
9.1.3 TIME VARYING FIELD - MOVING CIRCUIT

Both transformer emf and motional emf exist

$$V_{emf} = \oint \vec{E} \cdot d\vec{\ell} = \int_s -\frac{\partial \vec{B}}{\partial t} \cdot d\vec{s} + \oint (\vec{u} \times \vec{B}) \cdot d\vec{\ell}$$

Ex. 9.1 : A conducting bar moving on the rail is shown in the diagram. Find an induced voltage on the bar if :

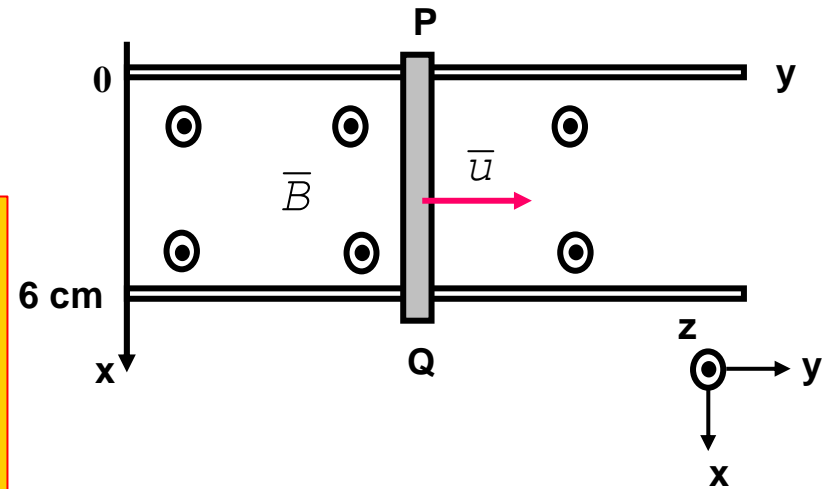
- (i) A bar position at $y = 8 \text{ cm}$ and $\bar{B} = 4 \cos 10^6 t \hat{z} \text{ mWb} / \text{m}^2$
- (ii) A bar moving with a velocity $\bar{u} = 20 \hat{y} \text{ m} / \text{s}$ and $\bar{B} = 4 \hat{z} \text{ mWb} / \text{m}^2$
- (iii) A bar moving with a velocity $\bar{u} = 20 \hat{y} \text{ m} / \text{s}$ and $\bar{B} = 4 \cos(10^6 t - y) \hat{z} \text{ mWb} / \text{m}^2$



Solution :

(i) Transformer case :

$$\begin{aligned} V_{emf} &= - \int \frac{\partial \bar{B}}{\partial t} \cdot d\bar{s} \\ &= \int_{y=0}^{0.08} \int_{x=0}^{0.06} 4(10^{-3})(10^6) \sin 10^6 t \, dx dy \\ &= 19.2 \sin 10^6 t \, (V) \end{aligned}$$



$$\bar{B} = 4 \cos 10^6 t \hat{z} \text{ mWb} / \text{m}^2$$

According to Lenz's law when \bar{B} increases point P will be at the higher potential with respect to point Q. (B induced will oppose the increasing \bar{B})

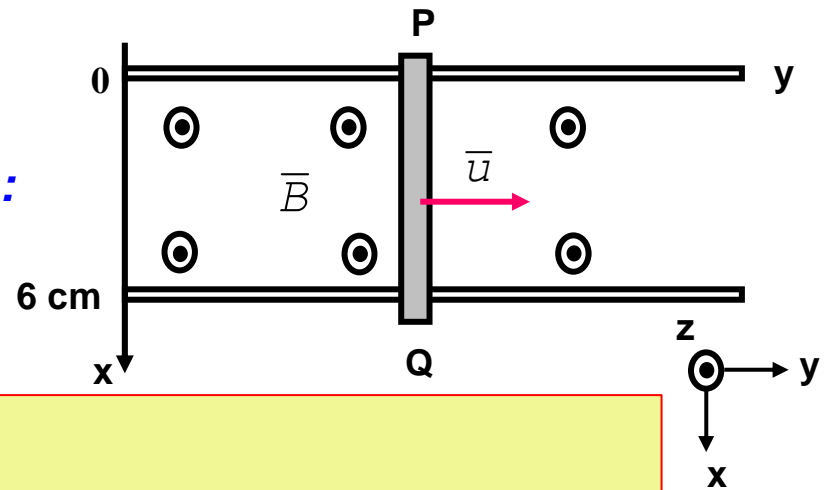
(ii) Motional case :

$$\begin{aligned} V_{emf} &= \int (\bar{u} \times \bar{B}) \cdot d\bar{\ell} \\ &= \int_{x=0}^{0.06} (20 \hat{y} \times 4 \hat{z}) \cdot dx \hat{x} \\ &= -4.8 \text{ mV} \end{aligned}$$

Remember : the direction of $d\bar{\ell}$ is opposed the current induced in the loop.

(iii) Both transformer and motional case :

$$\bar{B} = 4 \cos(10^6 t - y) \hat{z} \text{ mWb / m}^2$$



$$V_{emf} = - \int \frac{\partial \bar{B}}{\partial t} \cdot d\bar{s} + \int (\bar{u} \times \bar{B}) \cdot d\bar{\ell}$$

$$= \int_{x=0}^{0.06} \int_0^y 4(10^{-3})(10^6) \sin(10^6 t - y') dy' dx$$

$$+ \int_{0.06}^0 [20 \hat{y} \times 4(10^{-3}) \cos(10^6 t - y) \hat{z}] \cdot dx \hat{x}$$

$$= 240 \cos(10^6 t - y') \Big|_0^y - 80(10^{-3})(0.06) \cos(10^6 t - y)$$

$$= 240 \cos(10^6 t - y) - 240 \cos 10^6 t - 4.8(10^{-3}) \cos(10^6 t - y)$$

$$\approx 240 \cos(10^6 t - y) - 240 \cos 10^6 t$$

$$V_{emf} = - \int \frac{\partial \bar{B}}{\partial t} \cdot d\bar{s} + \int (\bar{u} \times \bar{B}) \cdot d\bar{\ell}$$
$$\approx 240 \cos(10^6 t - y) - 240 \cos 10^6 t$$

From trigonometry :

$$\cos A - \cos B = 2 \sin \frac{A + B}{2} \sin \frac{A - B}{2}$$

$$V_{emf} = 480 \sin \left(\left(10^6 t - \frac{y}{2} \right) \right) \sin \left(-\frac{y}{2} \right)$$

9.2 DISPLACEMENT CURRENT

From continuity of current equation :

$$\nabla \cdot \bar{J} = -\frac{\partial \rho_v}{\partial t} \quad \text{A/m}^3$$

and

$$\bar{J} = \nabla \times \bar{H}$$

$$\nabla \cdot \nabla \times \bar{H} = -\frac{\partial \rho_v}{\partial t} = -\frac{\partial}{\partial t} \nabla \cdot \bar{D} = -\nabla \cdot \frac{\partial \bar{D}}{\partial t} \quad \text{A/m}^3$$

$$\nabla \cdot \nabla \times \bar{H} = 0 = -\frac{\partial \rho_v}{\partial t} + \frac{\partial \rho_v}{\partial t} \quad ; \quad \text{and} \quad \nabla \cdot \bar{D} = \rho_v$$

Hence :

$$\nabla \cdot \nabla \times \bar{H} = \nabla \cdot \bar{J} + \frac{\partial}{\partial t} \nabla \cdot \bar{D}$$

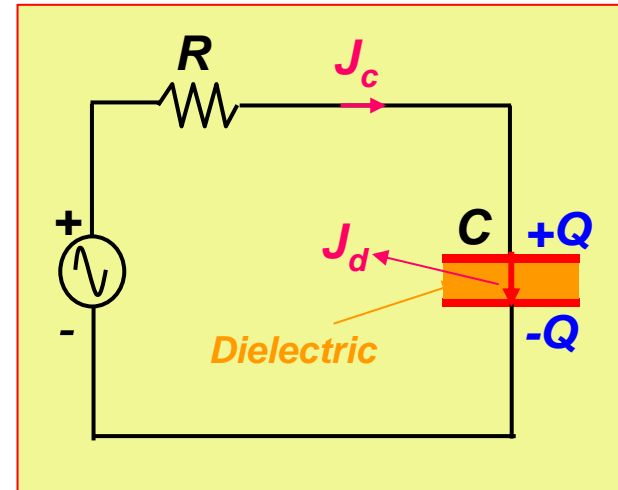
$$\nabla \cdot \nabla \times \bar{H} = \nabla \cdot \bar{J} + \frac{\partial}{\partial t} \nabla \cdot \bar{D}$$

$$\nabla \times \bar{H} = \bar{J} + \frac{\partial \bar{D}}{\partial t}$$

where :

\bar{J} = Conduction current density

$\frac{\partial \bar{D}}{\partial t}$ = Displacement current density



Hence :

$$\nabla \times \bar{H} = \bar{J}_c + \frac{\partial \bar{D}}{\partial t} = \bar{J}_c + \bar{J}_d$$

Therefore from *Faraday's law* and the concept of *displacement current* we can conclude that both the *magnetic and electric fields* are interrelated.

Maxwell's Equations

Differential Form	Integral Form	Label
$\nabla \times \bar{E} = -\frac{\partial \bar{B}}{\partial t}$	$\oint \bar{E} \cdot d\bar{\ell} = -\int \frac{\partial \bar{B}}{\partial t} \cdot d\bar{s}$	Faraday's Law
$\nabla \times \bar{H} = \bar{J} + \frac{\partial \bar{D}}{\partial t}$	$\oint \bar{H} \cdot d\bar{\ell} = I + \int \frac{\partial \bar{D}}{\partial t} \cdot d\bar{s}$	Ampere's Circuital Law
$\nabla \cdot \bar{D} = \rho_v$	$\oint_s \bar{D} \cdot d\bar{s} = \int_v \rho_v dv$	Gauss's Law for Electric Field
$\nabla \cdot \bar{B} = 0$	$\oint_s \bar{B} \cdot d\bar{s} = 0$	Gauss's Law for Magnetic Field

An **integral form** of Maxwell's equation can be found either by using **Divergence Theorem** or **Stoke Theorem**. All electromagnetic (EM) waves must conform or obey all the four Maxwell's equations.

Ex.9.2: A parallel plate capacitor having a plate area of 5 cm^2 and where the plates are separated by a distance of 3 mm is connected to a supply voltage, $50 \sin 10^3 t \text{ Volt}$. Calculate the displacement current if the dielectric permittivity between the plate is $\epsilon = 2\epsilon_0$.

Solution :

$$\overline{D} = \epsilon \overline{E} = \epsilon V / d$$

$$\overline{J}_d = \frac{\partial \overline{D}}{\partial t} = \frac{\epsilon}{d} \frac{\partial V}{\partial t}$$

$$\therefore I_d = \overline{J}_d \bullet d\overline{s}$$

$$= \frac{\epsilon S}{d} \frac{\partial V}{\partial t}$$

$$= 2\epsilon_0 \frac{5 \times 10^{-4}}{3 \times 10^{-3}} (10^3) 50 \cos 10^3 t$$

$$= 147.4 \cos 10^3 t \text{ nA}$$

This example is to show the use of Maxwell's equation and the inter relation of electric field and magnetic field.

Ex.9.3: Given a magnetic medium with characteristics $\sigma = 0, \mu = 2\mu_0, \varepsilon = 5\varepsilon_0$ has $\bar{H} = 2 \cos(\omega t - 3y) \hat{z}$ A / m . Find ω and \bar{E} .

Solution :

$$\nabla \times \bar{H} = \bar{J} + \frac{\partial \bar{D}}{\partial t} \quad ; \quad \sigma = 0$$

$$\nabla \times \bar{H} = \varepsilon \frac{\partial \bar{E}}{\partial t} \rightarrow \bar{E} = \frac{1}{\varepsilon} \int (\nabla \times \bar{H}) dt$$

$$\begin{aligned} \nabla \times \bar{H} &= \begin{vmatrix} \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ 0 & 0 & H_z \end{vmatrix} = \frac{\partial H_z}{\partial y} \hat{x} - \frac{\partial H_z}{\partial x} \hat{y} \\ &= 6 \sin(\omega t - 3y) \hat{x} \end{aligned}$$

$$\begin{aligned} \therefore \bar{E} &= \frac{1}{\varepsilon} \int 6 \sin(\omega t - 3y) dt \hat{x} \\ &= -\frac{1}{5\omega\varepsilon_0} 6 \cos(\omega t - 3y) \hat{x} \end{aligned}$$

$$\nabla \times \bar{E} = -\mu \frac{\partial \bar{H}}{\partial t}, \rightarrow \bar{H} = -\frac{1}{\mu} \int (\nabla \times \bar{E}) dt$$

$$\begin{aligned} \nabla \times \bar{E} &= \begin{vmatrix} \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ E_x & 0 & 0 \end{vmatrix} = -\frac{\partial E_x}{\partial z} \hat{y} + \frac{\partial E_x}{\partial y} \hat{z} \\ &= \frac{-3(6)}{5\omega\epsilon_0} \sin(\omega t - 3y) \hat{z} \end{aligned}$$

$$\begin{aligned} \bar{H} &= \frac{1}{\mu} \frac{18}{5\omega\epsilon_0} \int \sin(\omega t - 3y) dt \hat{z} \\ &= \frac{18}{10\omega\mu_0\epsilon_0} \cos(\omega t - 3y) \hat{z} \end{aligned}$$

$$\begin{aligned} \therefore \bar{E} &= \frac{1}{\epsilon} \int 6 \sin(\omega t - 3y) dt \hat{x} \\ &= -\frac{1}{5\omega\epsilon_0} 6 \cos(\omega t - 3y) \hat{x} \end{aligned}$$

Compare :

$$\begin{aligned} \bar{H} &= 2 \cos(\omega t - 3y) \hat{z} \text{ A/m} \\ \frac{18}{10\omega\mu_0\epsilon_0} &= 2 \\ \rightarrow \omega &= 2.846 \times 10^8 \text{ rad/s} \end{aligned}$$

Hence : $\bar{E} = -476.8 \cos(2.846 \times 10^8 t - 3y) \hat{x} \text{ (V/m)}$

9.3 LOSSY DIELECTRICS

Main function of *dielectric material* is to be used as an *insulator*.

For a *perfect dielectric* : $\sigma = 0$

Hence Maxwell's equation :

$$\begin{aligned}\nabla \times \bar{H} &= (\sigma + j\omega\epsilon')\bar{E} \\ \nabla \times \bar{H} &= j\omega\epsilon\bar{E} \quad (1)\end{aligned}$$

For *lossy dielectric* : $\sigma \neq 0$

$$\nabla \times \bar{H} = (\sigma + j\omega\epsilon')\bar{E} \quad (2)$$

Compare (1) and (2) :

$$\sigma + j\omega\epsilon' = j\omega\epsilon$$

$$\epsilon = \epsilon' - j\frac{\sigma}{\omega}$$

$$\epsilon = \epsilon' \left(1 - j\frac{\sigma}{\omega\epsilon'} \right) = \epsilon' - j\epsilon''$$

where :

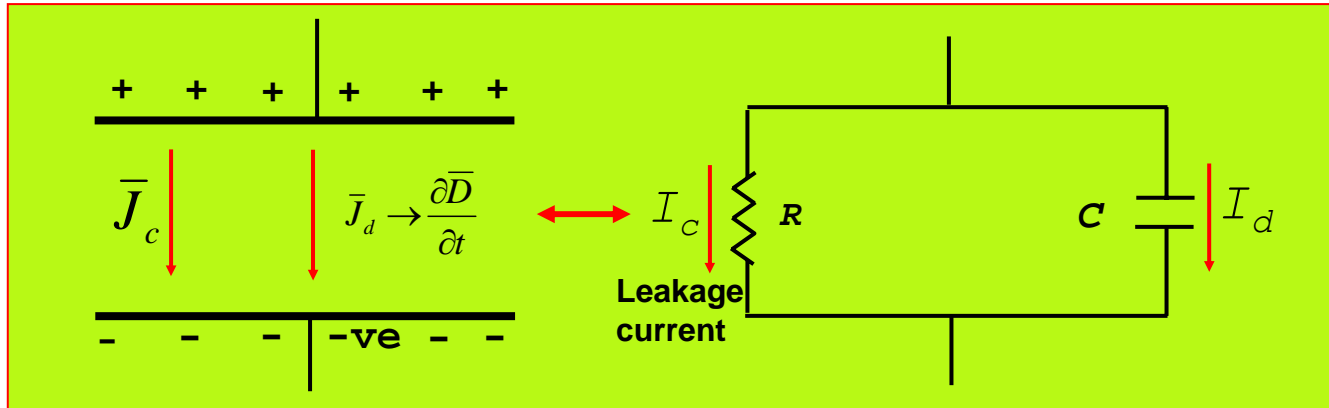
$$\sigma / \omega\epsilon' = \text{loss tangent}$$

Loss tangent is the ratio of the magnitude of the conduction current density to the magnitude of the displacement current density

$$= \frac{|I_c|}{|I_d|}$$

A **lossless capacitor** has a **loss tangent of zero**.

For **lossy capacitor**, an equivalent circuit can be replaced by its equivalent **resistance in parallel with a perfect capacitor** as shown in the diagram :



$$I_c = GV = \frac{V}{R} \quad \text{and} \quad I_d = j\omega CV$$

Hence **loss tangent** :

$$\frac{|I_c|}{|I_d|} = \frac{1/R}{\omega C} = \frac{\sigma s / d}{\omega \epsilon' s / d} = \frac{\sigma}{\omega \epsilon'} = \frac{\epsilon''}{\epsilon'}$$

From page 110 & 111

$$R = \frac{V}{I} = \frac{\int \bar{E} \cdot d\bar{l}}{\int \bar{J} \cdot d\bar{s}}$$

$$C = \frac{Q}{V} = \frac{\int \bar{D} \cdot d\bar{s}}{\int \bar{E} \cdot d\bar{l}}$$

Ex.9.4: Find the average power loss per unit volume for a capacitor having the following properties; dielectric constant 2.5 loss tangent 0.0005 for an applied electric field intensity of 1 kV/m at frequency 500 MHz.

Solution :

$$\text{Loss tangent} = 0.0005 = \frac{\sigma}{\omega \epsilon'}$$

$$\begin{aligned} \rightarrow \sigma &= (0.0005)(2\pi)(500 \times 10^6)(2.5\epsilon_0) \\ &= 3.476 \times 10^{-5} \text{ S / m} \end{aligned}$$

$$P = \frac{V^2}{2R} = \frac{V^2}{2 \frac{d}{\sigma s}} = \frac{1}{2} E^2 \sigma s d$$

$$\begin{aligned} \therefore \frac{P}{\text{volume}} &= \frac{1}{2} \sigma E^2 = \frac{1}{2} (3.476 \times 10^{-5})(10^3)^2 \\ &= 17.38 \text{ (W / m}^3\text{)} \end{aligned}$$

9.4 BOUNDARY CONDITIONS

Boundary conditions for *time varying field* are the same as boundary conditions in *electrostatics* and *magnetostatics* fields.

Tangential components for \bar{E} and \bar{H} :

$$E_{1t} = E_{2t} \quad ; \quad H_{1t} - H_{2t} = J_s$$

Normal components :

$$D_{1n} - D_{2n} = \rho_s \quad ; \quad B_{1n} = B_{2n}$$

If medium 2 is perfect conductor :

$$\bar{E} = \bar{H} = 0$$

Hence :

$$E_{1t} = 0 \quad ; \quad H_{1t} = J_s$$

$$D_{1n} = \rho_s \quad ; \quad B_{1n} = 0$$